

# Efficient and Accurate Scheme for Hyperbolic Conservation Laws

Mukkarum Hussain<sup>1</sup>, Ihtram ul Haq<sup>2</sup>, and Noor Fatima<sup>3</sup>

**Abstract**—The progress of numerical techniques for scalar and one dimensional Euler equation has been a great interest of researchers in the field of computational fluid dynamics for decades. In 1983, Harten worked on non-oscillatory first order accurate scheme and modified its flux function to obtain a second order accurate total variation diminishing (TVD) explicit difference schemes for scalar and one dimensional Euler equation. Although, TVD schemes are low dissipative and high resolution schemes, but for explicit formulation they are bounded by stability criterion  $CFL < 1$ . Stability criteria for explicit formulation limits time stepping and thus increase computational cost. Research in the field of efficient low dissipative high resolution scheme is an active ground. In 1986, Harten enhanced his TVD scheme and presented (2K+3) point explicit second order accurate schemes for scalar and one dimensional Euler equation which are TVD under CFL restriction  $K$ . Numerical experiments were made to demonstrate the performance of the schemes for several choices of  $K$ . His results depict that for increasing values of CFL total number of time steps are decreased which eventually decrease computational time. Computation of scalar problems depicts that Harten's large time step (LTS) scheme is a high resolution and efficient scheme. However, computations of hyperbolic conservation laws show some spurious oscillations in the vicinities of discontinuities for larger values of CFL. Zhan Sen Qian noticed that these spurious oscillations are due to the numerical formulation of the characteristic transformation used by Harten for extending the method for hyperbolic conservation laws. He suggested performing the inverse characteristic transformations by using the local right eigenvector matrix at each cell interface location to overcome these spurious oscillations. Large time step schemes developed by Harten and Qian have been tested with minmod limiter which is very dissipative. In present work, Qian MLTS TVD scheme is tested with more compressive limiters, namely, centralized MC and superbee. Shock tube problem for SOD boundary conditions is solved to understand the performance of MLTS TVD scheme with compressive limiters in the regions of discontinuities and strong shock waves.

**Keywords**—CFL, Explicit scheme, Large time step, Shock tube problem, TVD scheme, 1D Euler equation.

## I. INTRODUCTION

THE system of equation is called hyperbolic if it has all real and distinct Eigen values. Flow fields which are governed by hyperbolic equations are computed using marching

solutions. A scheme for hyperbolic system of equations is started with the given initial conditions and successively computes the flow field in marching direction [1] [2]. Transient 1D Euler equation is hyperbolic, no matter whether the flow is locally subsonic or supersonic. The marching direction for 1D Euler equation is the time direction. Methods to solve hyperbolic system of equations are primarily derived for non-linear wave equation and then implemented on hyperbolic system of equations.

Lax in 1954, modified Euler's Forward Time Central Space (FTCS) method and presented first-order accurate method to solve nonlinear wave equation. Lax method is stable for Courant-Friedrichs-Lewy condition (CFL) less than 1 and predicts the location of moving discontinuity correctly [1] [3]. This method is very dissipative and smears discontinuities over several mesh points and become worse as CFL decreases. Lax-Wendroff proposed a second-order accurate method for non-linear wave equation. His method sharply defined discontinuity and also stable for CFL less than 1 but produce undesirable oscillations when discontinuities are encountered. Similar to Lax method quality of results computed by Lax-Wendroff method degrade as CFL decrease [1].

Lax and Lax-Wendroff central finite difference schemes are stable and converge if flow field is sufficiently smooth but produce unwanted oscillations when discontinuities are met. It is due to the fact that series expansion for obtaining a difference approximation is only valid for continuous functions and has continuous derivatives at least through the order of difference approximation [4] [5]. Godunov recognized this deficiency and proposed a finite volume scheme instead of a finite difference scheme to avoid the need of differentiability. He used exact Riemann problem solution for evaluating the flux term at the cell interface. Computation of nonlinear wave equation is easily accomplished by using Godunov method but this method is very inefficient and take long time when applied to system of equations [1] [6]. To overcome this problem Roe suggested solving linear problem instead of actual nonlinear problem. Roe's approximate Riemann solver is efficient but cannot distinguish between expansion shock and compression shock. This is due to the violation of entropy condition and hence expansion shocks that are nonphysical may occur in computed results [7] [8]. A number of entropy fix have been recommended in literature to overcome this problem. Roe's upwind approximate Riemann solver capture physics in more appropriate way than Lax and Lax-Wendroff central schemes but is only first order accurate. Like second order central methods, higher order upwind

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methods have the same deficiencies and produce undesirable oscillations when discontinuities are encountered [9] [10].

Harten introduced the concept of Total Variation Diminishing (TVD) scheme. TVD schemes are monotonicity preserving schemes and therefore it must not create local extrema and the value of an existing local minimum must be non-decreasing and that of a local maximum must be non-increasing [1] [11] [12] [13]. He worked on non-oscillatory first order accurate scheme and modified its flux function to obtain a second order accurate total variation diminishing (TVD) explicit difference schemes for scalar and system of hyperbolic conservation laws. Numerical dissipation terms in TVD methods are nonlinear. The quantity varies from one grid point to another and usually consists of automatic feedback mechanisms to control the amount of numerical dissipation. After this breakthrough a number of TVD scheme have been proposed and discussed in literature [14] [15] [16] [17] [18].

Stability criteria for explicit formulation limits time stepping and thus increase computational cost. Similar to previously discussed schemes, explicit formulation of Harten and other TVD schemes are also stable only for Courant-Friedrichs-Lewy condition (CFL) less than 1. It is a challenging task to develop an explicit scheme which is stable for higher values of CFL number. In literature this kind of schemes are known as large time step (LTS) schemes and an active field of research for last three decades. Leveque described a method for approximating nonlinear interactions linearly which allows Godunov's method to be applied with arbitrarily large time steps [18] [19]. Harten extended Leveque work and proposed second-order accurate total variation diminishing large time step explicit schemes for the computation of hyperbolic conservation laws. Computation of nonlinear wave equation depicts that Harten's LTS scheme is a high resolution and efficient scheme [21]. However, computation of system of hyperbolic conservation laws show some spurious oscillations in the vicinities of discontinuities when  $CFL > 1$ . Zhan Sen Qian worked on Harten LTS TVD scheme and observed that these spurious oscillations are due to the numerical formulation of the characteristic transformation used by Harten for extending the method for hyperbolic conservation laws [22] [23] [24]. Zhan Sen Qian showed that if the inverse characteristic transformations are performed by using the local right eigenvector matrix at each cell interface location then these spurious oscillations are eliminated. His computations for shock tube problem confirm that the modified large time step total variation diminishing (MLTS TVD) scheme eliminate spurious oscillations for system of hyperbolic conservation laws without increasing the entropy fixing parameter.

Harten and Qian developed large time step schemes have been tested with minmod limiter which is very dissipative. In present work, Qian MLTS TVD scheme is tested with more compressive limiters, namely, centralized MC [25] and superbee [8]. Shock tube problem for SOD boundary conditions [26] is solved to understand the performance of MLTS TVD scheme with compressive limiters in regions of discontinuities and strong shock waves. Shock tube problem is

often used by researcher to evaluate the performance of different schemes. Reasons of attraction in this test case are availability of analytical solution and at the same time presence of complex flow feature namely, expansion, shock wave, and contact discontinuities.

## II. NUMERICAL METHOD

In this paper 1D transient Euler equation in a conservation form is used:

$$\frac{\partial U}{\partial t} + \frac{\partial F}{\partial x} = 0 \quad (1)$$

$$\frac{\partial U}{\partial t} + A \frac{\partial U}{\partial x} = 0 \quad (2)$$

where

$$U = \begin{bmatrix} \rho \\ \rho u \\ \rho E \end{bmatrix}; \quad F = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ (\rho E + p)u \end{bmatrix} \quad (3)$$

$$A = \frac{\partial F}{\partial U} = \begin{bmatrix} 0 & 1 & 0 \\ (\gamma - 3)\frac{u^2}{2} & (3 - \gamma) & (\gamma - 1) \\ (\gamma - 1)u^3 - \gamma u E & -\frac{3}{2}(\gamma - 1)u^2 + \gamma E & \gamma u \end{bmatrix} \quad (4)$$

equation (1) in numerical flux form can be written as:

$$U_i^{n+1} = U_i^n - \lambda \left( f_{i+\frac{1}{2}}^n - f_{i-\frac{1}{2}}^n \right) \quad (5)$$

where  $\lambda = \frac{\Delta x}{\Delta t}$

Harten used Leveque's scheme [19] [20] and proposed large time step TVD scheme which is second order accurate using  $(2K + 3)$  points explicit discretization for hyperbolic conservation laws and increasing the CFL restriction upto  $K$  [21]. The numerical flux for Harten's LTS TVD is given by:

$$f_{i+\frac{1}{2}} = \frac{1}{2} [F_{i+1} + F_i] + \frac{1}{2\lambda} \sum_{k=1}^m R_{i+\frac{1}{2}}^k (g_{i+1}^k + g_i^k) - \frac{1}{\lambda} \sum_{k=1}^m R_{i+\frac{1}{2}}^k \left[ \sum_{l=-K+1}^{K-1} C_l (v^k + \gamma^k)_{i+\frac{1}{2}} \alpha_{i+\frac{1}{2}}^k \right] \quad (6)$$

here;

$$v_{i+\frac{1}{2}}^k = \lambda a_{i+\frac{1}{2}}^k \quad (7)$$

$$\alpha_{i+\frac{1}{2}} = R^{-1} \Delta_{i+\frac{1}{2}} U \quad (8)$$

$$\tilde{g}_{i+\frac{1}{2}}^k = \frac{1}{2} \left\{ Q \left( v_{i+\frac{1}{2}}^k \right) - \left( v_{i+\frac{1}{2}}^k \right)^2 \right\} \alpha_{i+\frac{1}{2}}^k \quad (9)$$

$$\gamma_{i+\frac{1}{2}}^k = \begin{cases} \frac{(g_{i+1}^k - g_i^k)}{\alpha_{i+\frac{1}{2}}^k}, & \alpha_{i+\frac{1}{2}}^k \neq 0 \\ 0, & \alpha_{i+\frac{1}{2}}^k = 0 \end{cases} \quad (10)$$



Courant number. Slight oscillation is present near contact discontinuity for centralized MC and superbee limiters. Oscillations become worse as Courant number increases. Extant of spurious oscillation is greater for centralized MC limiter results as compare to super bee limiter. For smaller values of Courant number ( $CFL \leq 2$ ) minmod limiter produces oscillation free results across shock and contact discontinuity. Although for larger values of Courant number ( $CFL > 2$ ) minmod limiter also produces oscillation near contact discontinuity but the extant of oscillation produces by minmod limiter is not as much as compare to other two limiters. Results computed using centralized MC and superbee limiters near shock and contact discontinuities are less dissipative as compare to minmod limiter.

Higher pressure side of expansion fan is found oscillation free with all three limiters for different values of K and Courant number. Slight oscillation is present near lower pressure side of expansion fan. Oscillations become worse as Courant number increases. Extant of spurious oscillation is greater for centralized MC limiter results as compare to super bee limiter. Minmod limiter produces minimum oscillatory results near lower pressure side of expansion fan.

Results for super bee limiter taking  $K = 1, 2, 3,$  and  $4$  for  $0.8, 1.8, 2.8,$  and  $3.8$  values of Courant number respectively are also compared and analyzed in Figure 17-20. Computed results of density profile are plotted at shock, contact and expansion fan regions along with analytical results. Results near shock discontinuity are oscillation free for all values of Courant number. For  $K=1$ , predicted shock discontinuity is behind the analytically calculated shock discontinuity. Predicted shock discontinuity travel in the direction of shock as  $K$  increases. For  $K=4$ , predicted shock discontinuity surpasses analytically calculated shock discontinuity and it is in front of it. Spurious oscillation is noticed near contact discontinuity. Oscillation is found to be a function of Courant number and it increases as Courant number increases. Results also depict that dissipation across expansion fan widen as Courant number increases.

Computed results near shock wave region for a particular limiter with a specific value of Courant number are superior to contact discontinuity. This is due to the fact that characteristic lines near shock wave are convergent while near contact discontinuity they are parallel to each other. Convergent nature of characteristic lines minimizes dissipation near shock region. The computed results are in good agreement with analytical results with all three limiters for different values of  $K$  and Courant number apart from slight oscillations near contact discontinuity for large values of  $K$ .

Computed results depict that the difference between analytical and numerical results near expansion fan, contact and shock discontinuities increase for larger values of Courant number. Increase in discrepancy might be due to the increase in truncation error. Sine truncation error strongly depends on step size and time step size increase as Courant number increase.

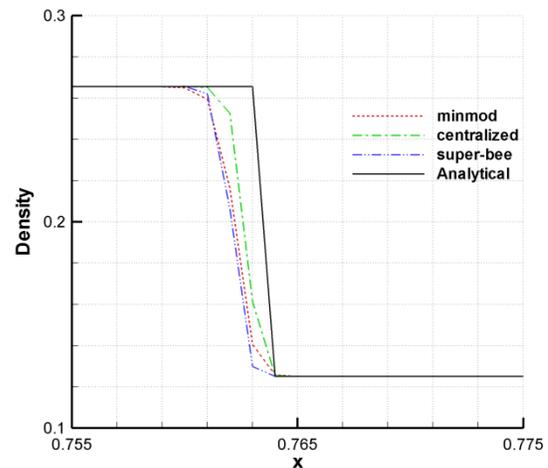


Figure 1: NearShock Region, K=1, CFL=0.8

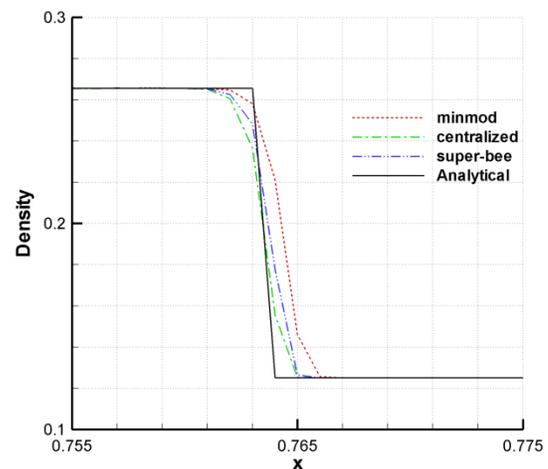


Figure 2: Near Shock Region, K=2, CFL=1.8

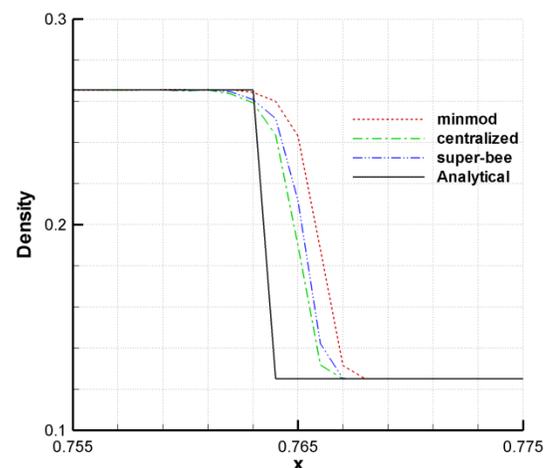


Figure 3: Near Shock Region, K=3, CFL=2.8

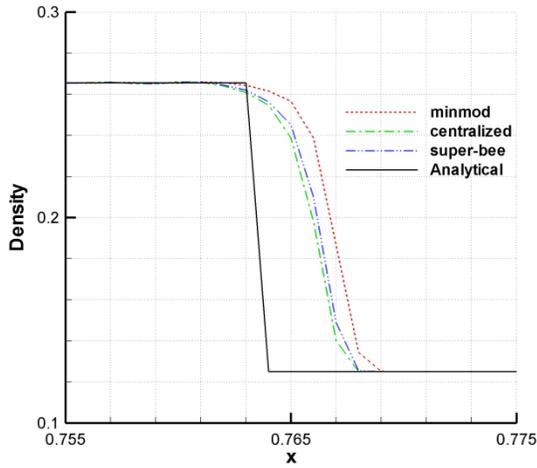


Figure 4: Near Shock Region,  $K=4$ ,  $CFL=3.8$

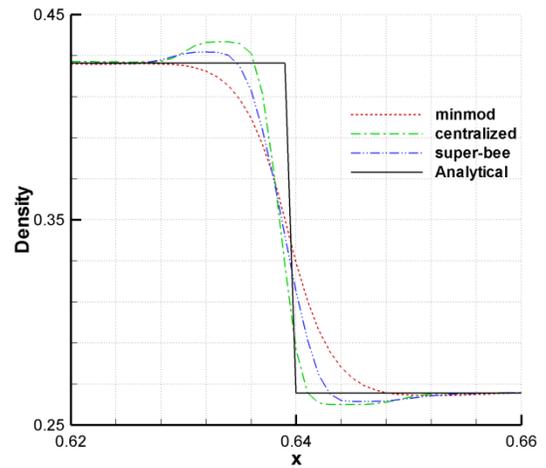


Figure 7: Near Contact Region,  $K=3$ ,  $CFL=2.8$

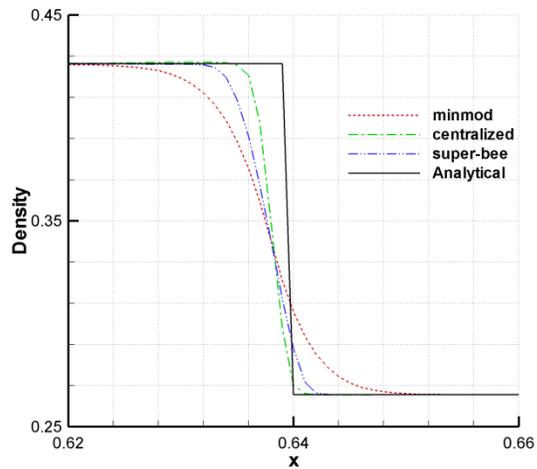


Figure 5: Near Contact Region,  $K=1$ ,  $CFL=0.8$

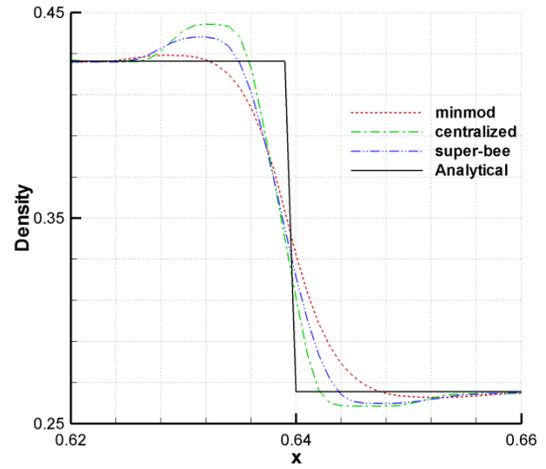


Figure 8: Near Contact Region,  $K=4$ ,  $CFL=3.8$

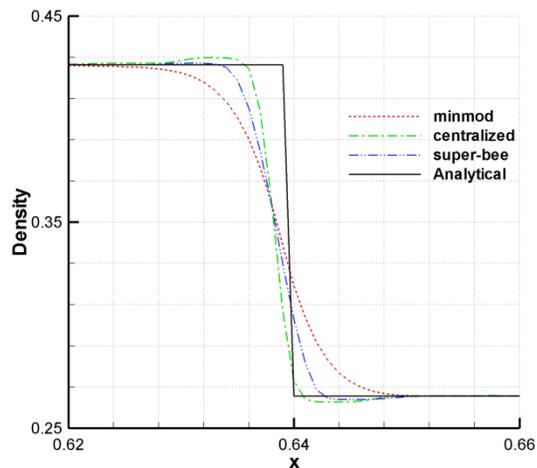


Figure 6: Near Contact Region,  $K=2$ ,  $CFL=1.8$

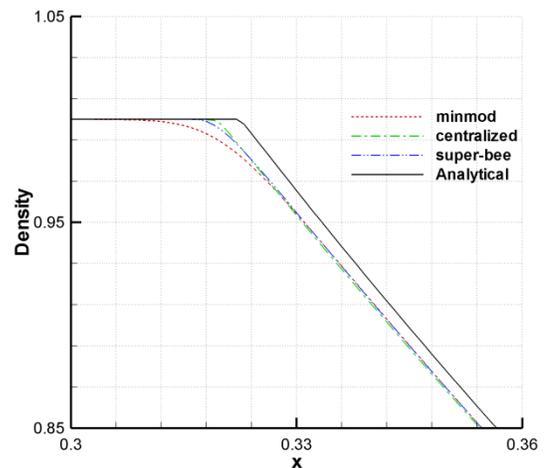


Figure 9: Near Start of Expansion Wave Region,  $K=1$ ,  $CFL=0.8$

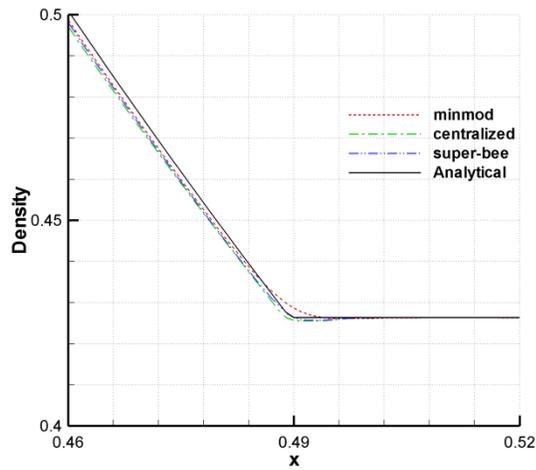


Figure 10: Near End of Expansion Wave Region,  $K=1$ ,  $CFL=0.8$

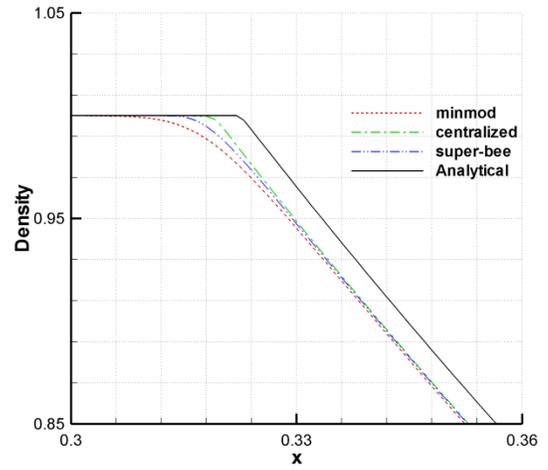


Figure 13: Near Start of Expansion Wave Region,  $K=3$ ,  $CFL=2.8$

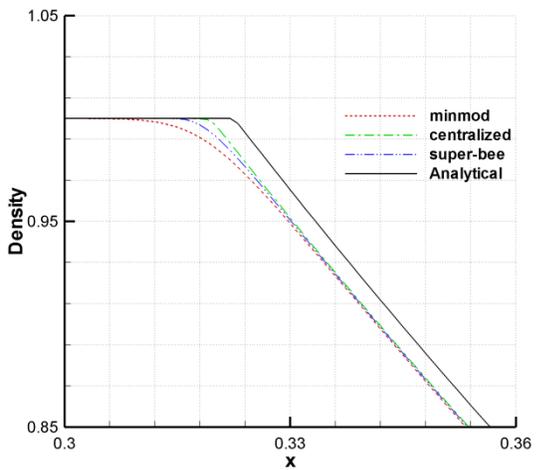


Figure 11: Near Start of Expansion Wave Region,  $K=2$ ,  $CFL=1.8$

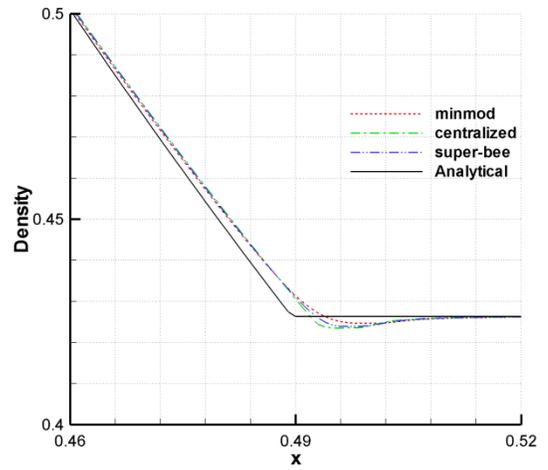


Figure 14: Near End of Expansion Wave Region,  $K=3$ ,  $CFL=2.8$

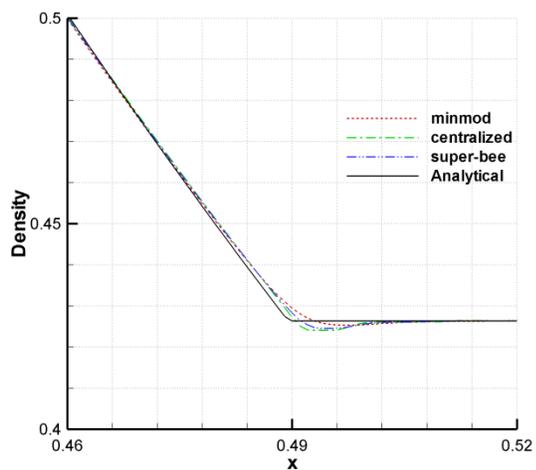


Figure 12: Near End of Expansion Wave Region,  $K=2$ ,  $CFL=1.8$

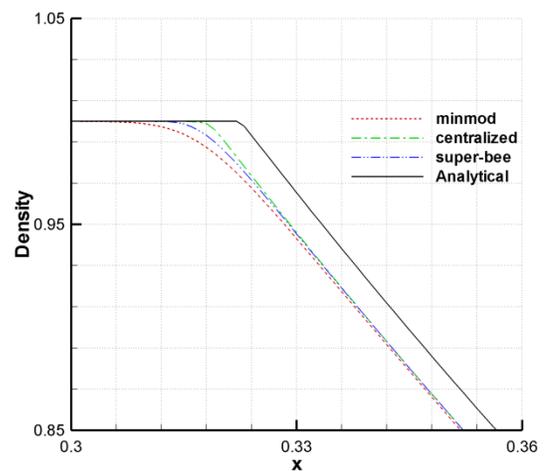


Figure 15: Near Start of Expansion Wave Region,  $K=4$ ,  $CFL=3.8$

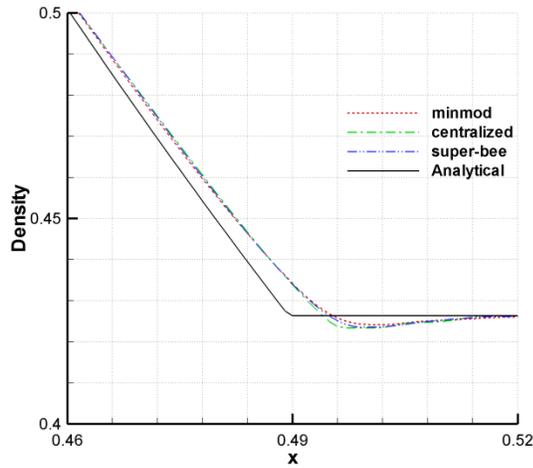


Figure 16: Near End of Expansion Wave Region, K=4, CFL=3.8

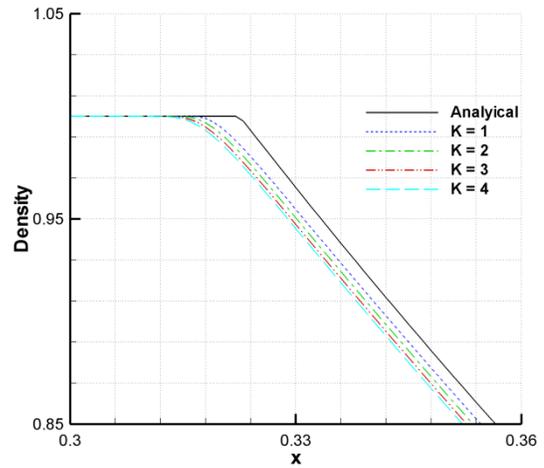


Figure 19: Near Start of Expansion Wave Region, superbee limiter

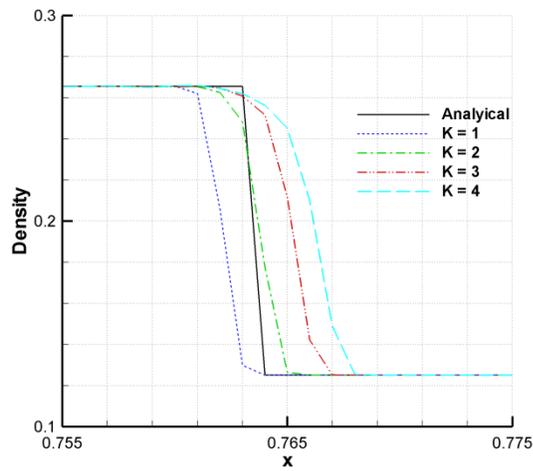


Figure 17: Near Shock Region, superbee limiter

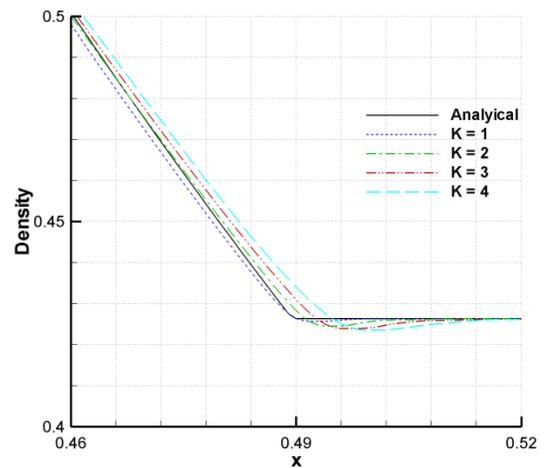


Figure 20: Near End of Expansion Wave Region, superbee limiter

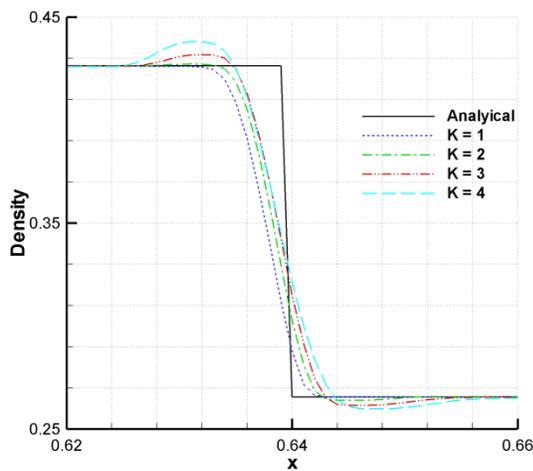


Figure 18: Near Contact Region, superbee limiter

### V. CONCLUSION

In present work Qian MLTS TVD scheme is tested with more compressive limiters, namely, centralized MC and superbee. Shock tube problem for SOD boundary conditions is solved to understand the performance of MLTS TVD scheme with compressive limiters in the regions of discontinuities and strong shock waves. Recent results suggested that MLTS TVD scheme is remain stable for compressive limiter. For all three limiters some oscillations are found near contact and lower pressure side of expansion fan. As expected, it is noticed that minmod limiter produces least oscillation while oscillations are larger for centralized MC limiter as compare to super bee limiter. Results also depicts that centralized MC and super bee limiters are less dissipative as compare to minmod limiter, which is due to the compressive nature of former two limiters.

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